



PCT/AU03/01465

REC'D 21 NOV 2003

WIPO

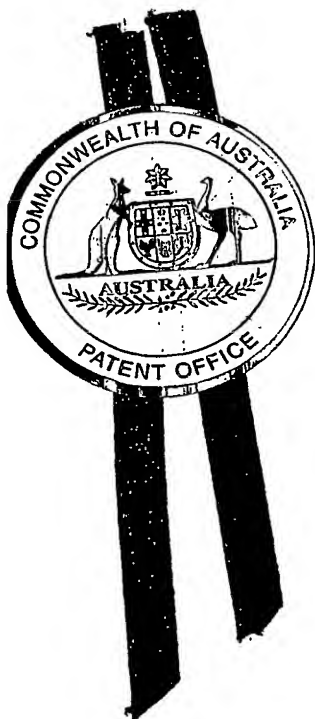
PCT

**PRIORITY  
DOCUMENT**

SUBMITTED OR TRANSMITTED IN  
COMPLIANCE WITH RULE 17.1(a) OR  
(b)

**Patent Office  
Canberra**


I, JANENE PEISKER, TEAM LEADER EXAMINATION SUPPORT AND  
SALES hereby certify that annexed is a true copy of the Provisional specification  
in connection with Application No. 2002952531 for a patent by TELSTRA  
CORPORATION LIMITED as filed on 06 November 2002.



WITNESS my hand this  
Seventeenth day of November 2003

JANENE PEISKER  
TEAM LEADER EXAMINATION  
SUPPORT AND SALES

BEST AVAILABLE COPY



Regulation 3.2

**Telstra Corporation Limited**

**A U S T R A L I A**

***Patents Act 1990***

**PROVISIONAL SPECIFICATION**

for the invention entitled:

**"A TRANSMIT ANTENNA"**

The invention is described in the following statement:

- 1 -

## A TRANSMIT ANTENNA

### FIELD OF THE INVENTION

The present invention relates to a transmit antenna, and in particular to an antenna for  
5 transmitting signals for high frequency surface wave radar.

### BACKGROUND

High frequency surface wave radar (HFSWR) systems have been developed to overcome  
the line-of-sight limitation of microwave radar systems. HFSWR exploits a phenomenon  
10 known as a Norton wave propagation whereby a vertically polarised electromagnetic signal  
propagates efficiently as a surface wave along a conducting surface. HFSWR systems  
operate from coastal installations, with the ocean providing the conducting surface. The  
transmitted signal follows the curved ocean surface, and a system can detect objects  
beyond the visible horizon, with a range of the order of 300 km.

15

As shown in Figure 1, a surface wave radar system includes a transmitter 12, and a  
receiver 14. The transmitter 12 includes transmitter electronics 18 and a transmitting  
antenna 16. The transmitting antenna 16 is a directional broadband antenna, such as a log-  
periodic antenna array, capable of generating a substantial surface wave and a relatively  
20 insubstantial overhead skywave. The transmitting antenna 16 transmits high frequency (5-  
10 MHz) electromagnetic surface wave signals from a shoreline 26 across the ocean  
surface. The transmitted signals are reflected from objects such as a ship 28, and reflected  
surface wave signals are received by the receiver 14.

25 The receiver 14 includes a data processing system 24 and a broadside array 20 of vertically  
polarised antenna doublets. The broadside array 20 is oriented approximately  
perpendicular to a principal receiving direction 25 for reflected surface wave signals, and,  
in this case, is approximately parallel to the shore 26. The receiver 14 can also include an  
endfire array 22 of vertically polarised monopole antenna elements, oriented perpendicular

and adjacent to the broadside array 20 to form a two-dimensional (2-D) receiving antenna array.

A standard log-periodic antenna array is suitable for the directional transmission of vertically polarised signals over a wide bandwidth and beam width. However, it is often necessary to transport the antenna to various locations. Log-periodic antenna arrays designed for these frequencies (5-10 MHz) are large and expensive structures that require considerable effort for disassembly, transportation, site preparation and reassembly. It is desired, therefore, to provide a transmit antenna that alleviates one or more of these difficulties, or at least provides a useful alternative to existing transmit antennas.

#### SUMMARY OF THE INVENTION

In accordance with the present invention, there is provided a transmit antenna for a surface wave radar system, including:

- 15 a linear array of active monopole antenna elements for transmitting signals in respective frequency ranges, the relative spacings and the relative heights of successive elements along the array having substantially logarithmic relationships;
  - impedance matching circuits for the active monopole antenna elements; and
  - switches for selecting one of the active antenna elements to transmit a signal in a
- 20 corresponding frequency range while grounding the remaining active antenna elements.

Advantageously, the switches may sequentially select one of said elements. The sequential switching may be continuous and repeated.

- 25 Preferably, the antenna includes a passive element at each end of the array, wherein the relative heights and relative spacings of each passive element and its adjacent active element have logarithmic relationships.

Preferably, each active antenna element includes a radial wire counterpoise.

## BRIEF DESCRIPTION OF THE DRAWINGS

A preferred embodiment of the present invention is hereinafter described, by way of example only, with reference to the accompanying drawings, wherein:

Figure 1 is a schematic diagram of a surface wave radar system;

5        Figures 2 to 4 are schematic diagrams of a preferred embodiment of a transmitting antenna of the radar system;

Figure 5 is a graph of VSWR as a function of frequency for each impedance matched antenna; and

10        Figures 6 to 11 are graphs of the simulated and measured radiation patterns from each antenna element with impedance matching, at frequencies of 5.1, 6.1, 7.1, 8.1 9.1, and 10.2 MHz, respectively.

## DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

As shown in Figure 2, a transmit antenna 16 includes a linear array of four active base-fed  
15        monopole antenna elements 30 to 36 and two passive elements 38, 40, one at each end of the array. Each of the active monopole elements 30 to 36 transmits signals in a unique portion of the antenna's 5–10 MHz frequency transmission range, as shown in Table 1.

Table 1

element	height (m)	position (m)	frequency range (MHz)
passive reflector (40)	16.00	0	—
Element 1 (30)	12.78	13.94	5.0–5.7
Element 2 (32)	10.75	25.66	5.7–7.1
Element 3 (34)	9.04	35.52	7.1–8.15

Element 4 (36)	7.60	43.81	8.15-10.0
passive director (38)	6.39	50.78	—

The tallest passive element 40 is a sixteen metre wind-up lattice mast and acts as a reflector at the low frequency end of the antenna's operating frequency range. The other passive element 38 is shorter and acts as a director at the high frequency end of the antenna's operating frequency range. The six elements 30 to 40 have logarithmic relationships in height and position within the antenna array, as can be determined from the data of Table 1 below. The specific values for the heights and positions are determined using standard antenna design software such as numerical electromagnetic code (NEC) and SPICE.

A grounded radial wire counterpoise under each antenna element reduces ground losses and stabilises the impedance of each antenna element 30 to 36 under varying ground conditions. The configurations of the counterpoises are shown in a plan view of the transmit antenna 16 in Figure 3. Viewed from above, the nine wires of each counterpoise extend radially from one side of the base of the corresponding antenna element, each adjacent pair of wires separated by an angle  $\phi = 22.5^\circ$ . Table 2 provides the lengths of the counterpoise wires.

Table 2

Wire	Length (m)	Wire	Length (m)
A	13.9	I	13.27
B	17	J	10.16
C	20	K	7.846
D	16	L	11.4
E	11.27	M	8.73
F	16.25	N	6.52

- 5 -

G	12.45	O	9.54
H	9.16	P	7.3

As shown in Figure 4, the antenna includes interface modules 42 to 48 for interfacing the respective monopole elements 30 to 36 to the transmitter electronics 18. The interface modules 42 to 48 each include a respective two or three element LC impedance matching network 50 to 56 and a standard high-power latching radio-frequency (RF) power relay or switch 58. The impedance matching networks 50 to 56 each include a respective capacitor 60 to 66 and inductor 68 to 74 in parallel with the transmitter signal; the first 42 and third 46 networks also include an additional inductor 76, 78 in series with the signal.

The RF switches 58 allow each antenna to be independently connected to the transmitter electronics 18 via the coaxial cable 76, or shorted to ground potential. When a signal of a particular frequency is transmitted, the antenna whose allotted frequency range includes that frequency is connected to the transmitter electronics 18, and the remaining three antennas are shorted to ground. This switching is performed by remotely controlling the switches 58 to 64 by sending appropriate signals on control cables 80. A 24-volt gate pulse sent to one of the RF switches 58 to 64 on that switch's control cable activates the RF switch to connect the coaxial cable 76 to the corresponding interface module (e.g., the second interface module 44), and thereby to the corresponding antenna (e.g., the second antenna 32). The other antenna elements are shorted to ground and act as additional reflectors or directors.

Table 3 provides details of the values of capacitance and inductance for each of the active antenna element matching networks 50 to 56.

Table 3

element	parallel capacitance (pF)	series inductance ( $\mu$ H)	parallel inductance ( $\mu$ H)
passive reflector (40)	—	—	—
Element 1 (30)	2578	—	0.339
Element 2 (32)	1557.4	0.574	0.438
Element 3 (34)	1276.8	—	0.330
Element 4 (36)	1339.5	0.400	0.244
passive director (38)	—	—	—

- 5 As shown in Figure 5, the voltage standing wave ratios (VSWRs) 601 to 604 for the four antenna elements are predominantly between 1.2:1 and 1.4:1 over the entire operating frequency range of the antenna.

Figures 5 to 10 show measured 701 and simulated 702 azimuthal radiation patterns for the antenna array at frequencies of 5.1, 6.1, 7.1, 8.1 9.1, and 10.2 MHz, respectively. The simulated patterns include antenna and mismatch losses and appear to match the measured patterns closely. Some discrepancies are apparent at the higher frequencies, probably due to factors such as adjacent buildings and structures that affect surface-wave attenuation.

- 15 The antenna 16 is designed to have a limited frequency range of 5–10 MHz, but the high-frequency characteristics of the array can be extended by adding one or more active elements to the high-frequency end of the array. This slightly increases the gain of the fourth antenna element 36 without significantly affecting its impedance.



- 7 -

In comparison with a standard log-periodic antenna array, the logarithmic monopole antenna array 16 has a lower gain and broader azimuth and elevation radiation patterns. However, the cost of manufacture is greatly reduced, and the logarithmic monopole antenna is readily transportable.

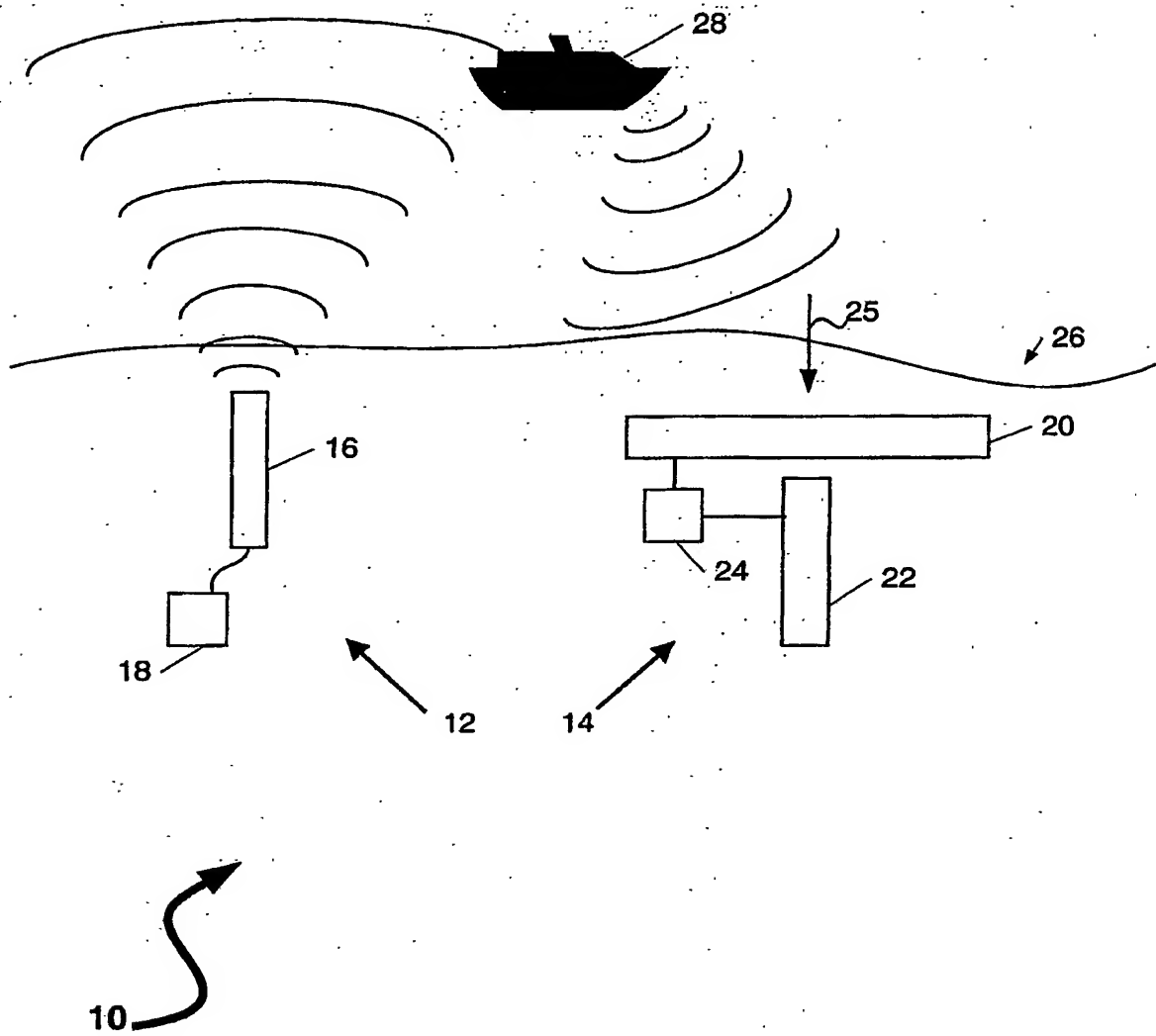
Many modifications will be apparent to those skilled in the art without departing from the scope of the present invention as herein described with reference to the accompanying drawings.

10

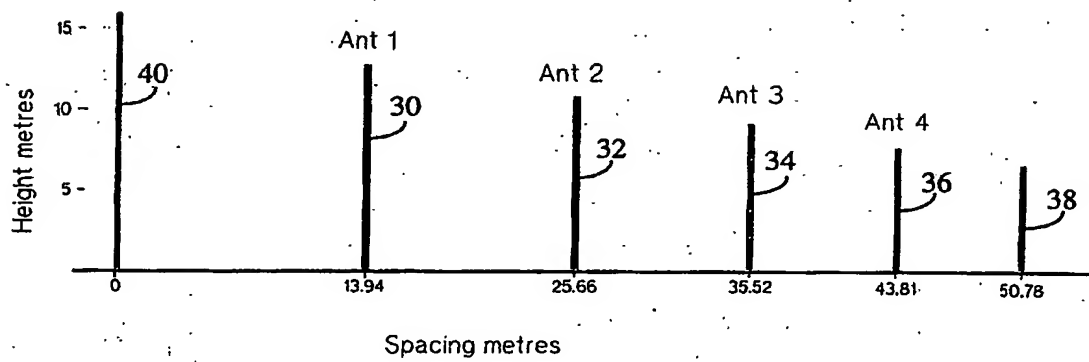
DATED this 6th day of November, 2002

15

**Telstra Corporation Ltd**  
By its Patent Attorneys  
**DAVIES COLLISON CAVE**



**Figure 1**



**Figure 2**

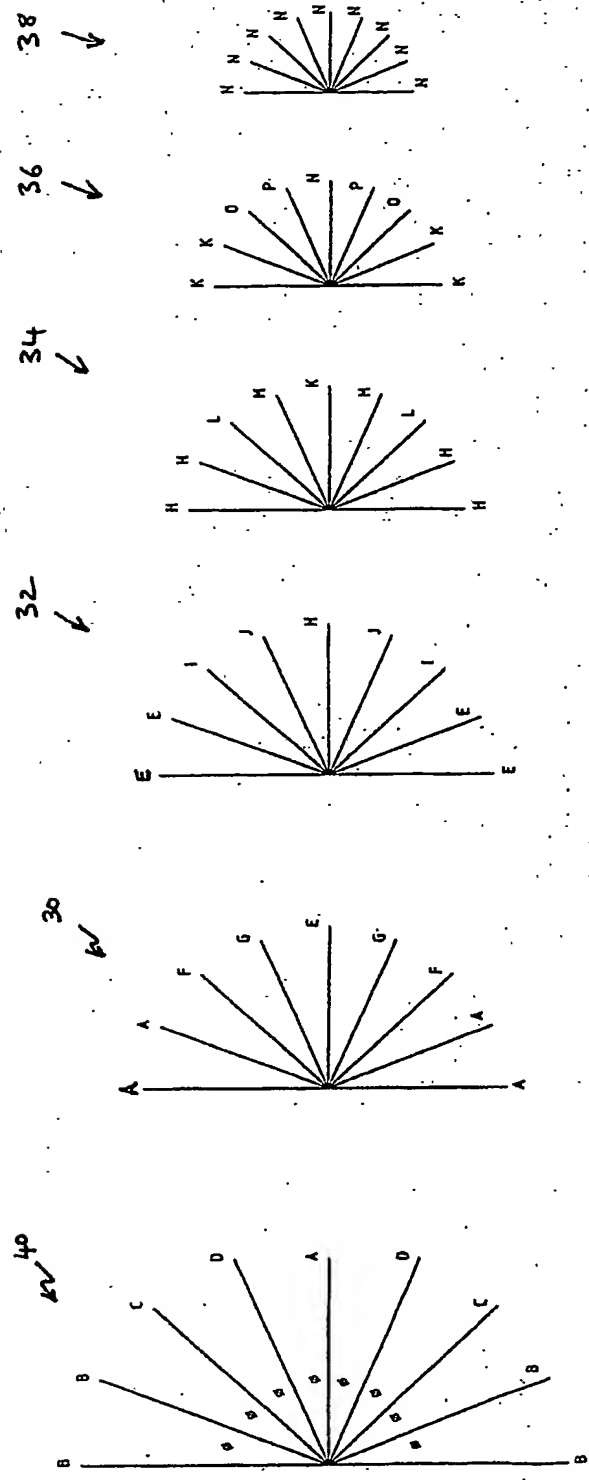


Figure 3

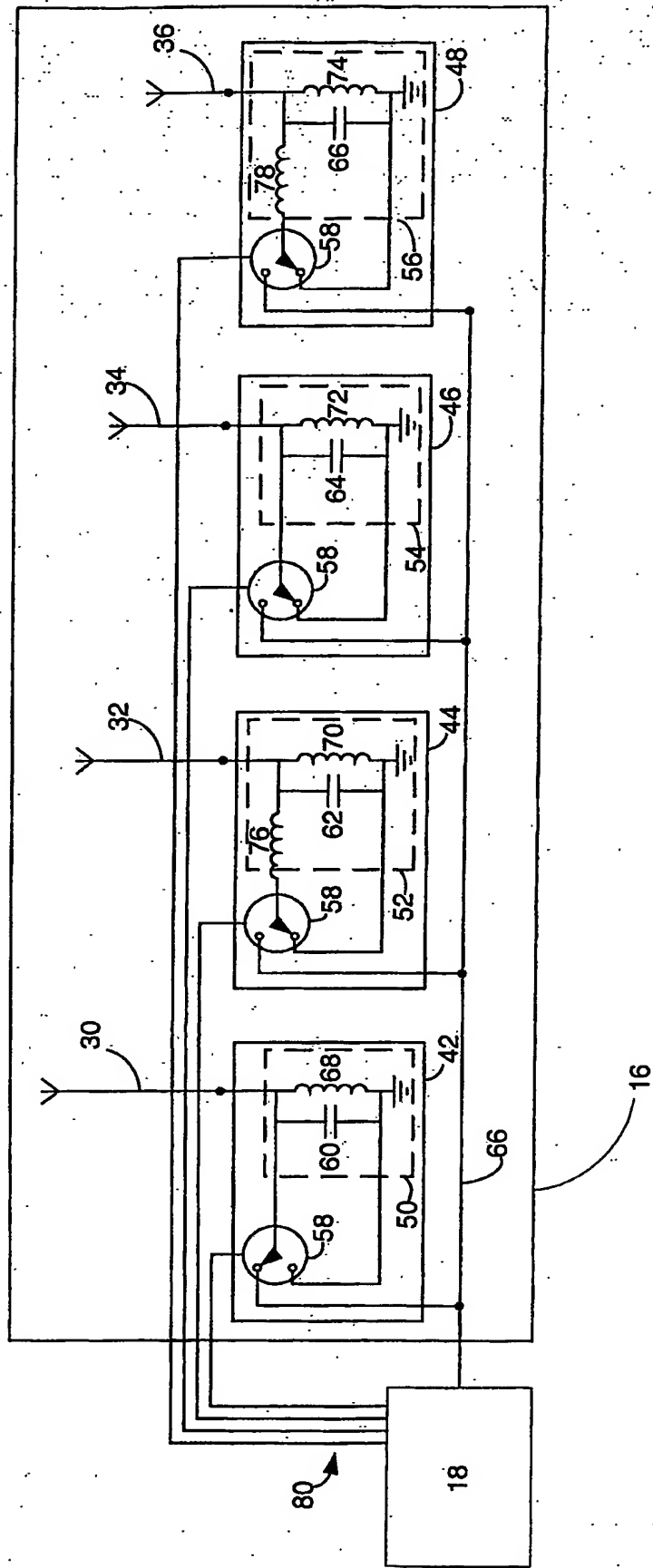


Figure 4

# Log-periodic Monopole Antenna.

Matched VSWR.

Antenna 1.  
VSWR

Antenna 2.  
VSWR

Antenna 3.  
VSWR

Antenna 4.  
VSWR

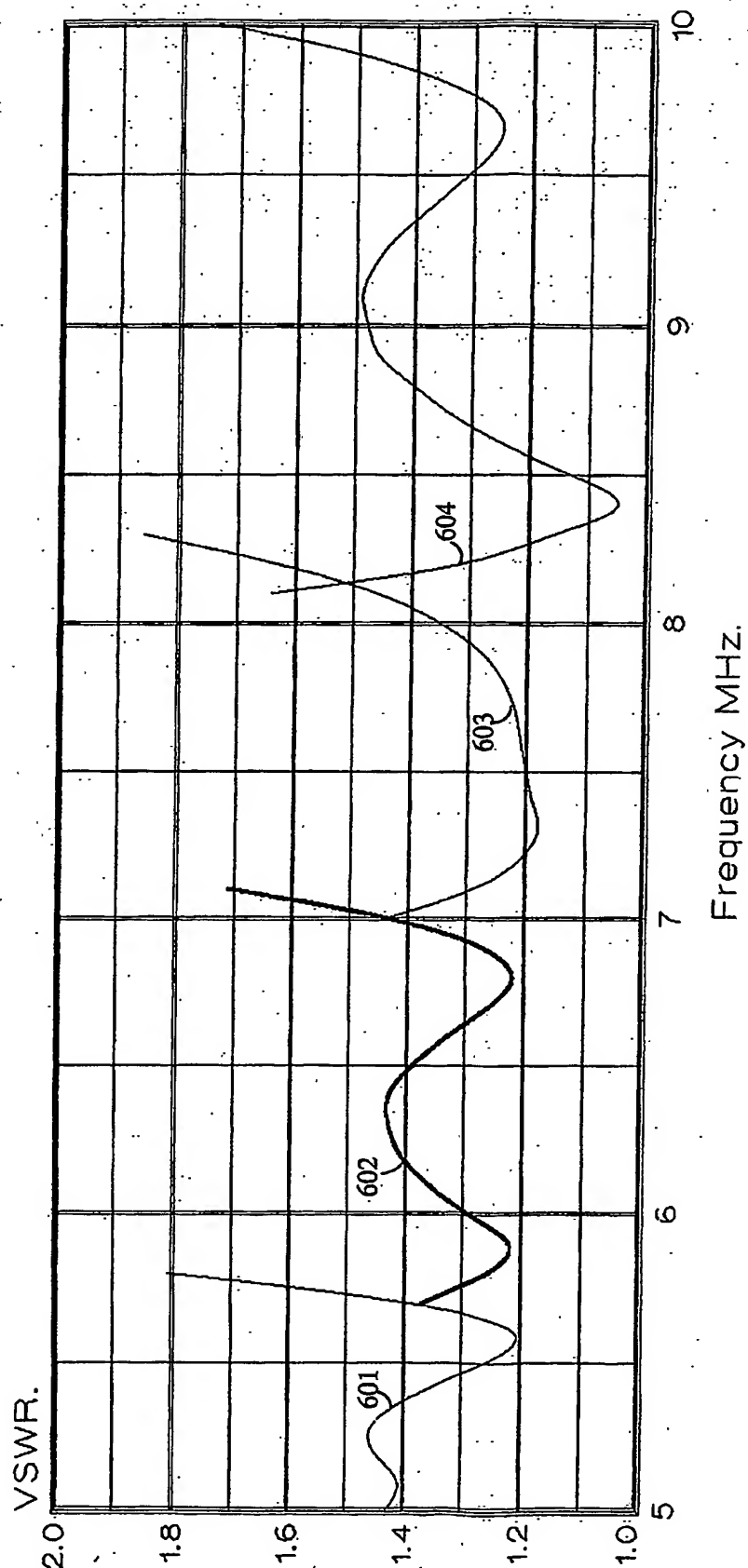


Figure 5

# Log-periodic Monopole Antenna. Azimuth Pattern at 5.1 MHz.

Pattern  
Calculated

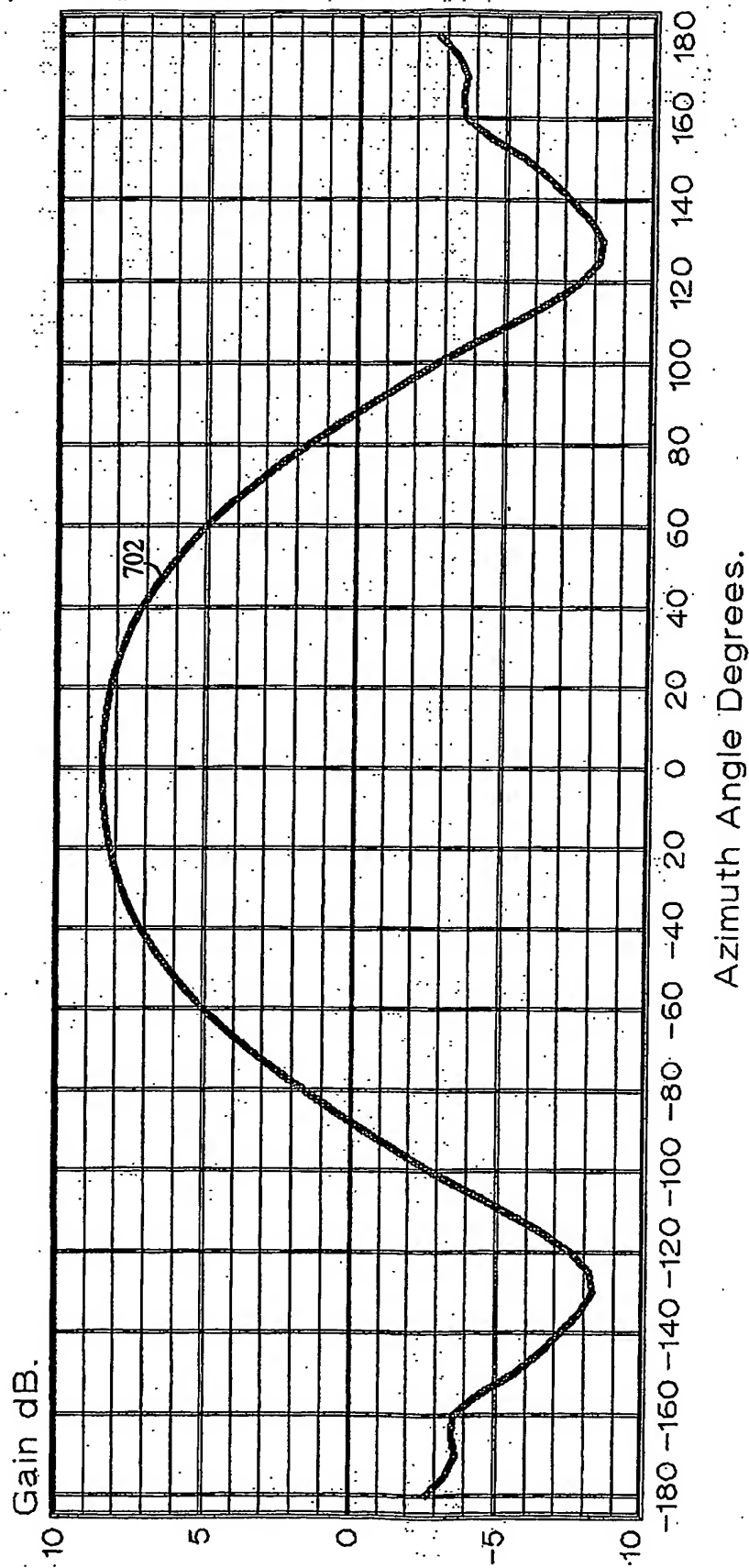
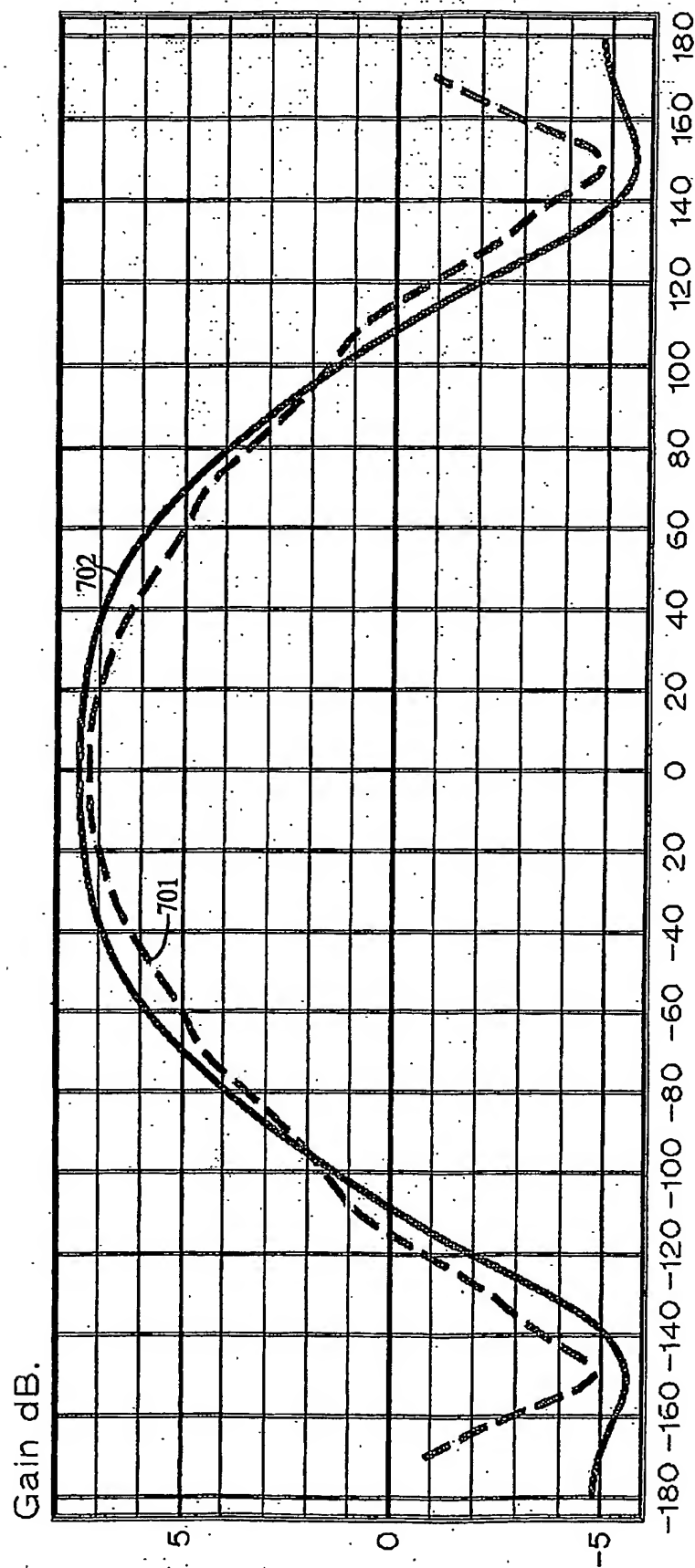


Figure 6

# Log-periodic Monopole Antenna. Azimuth Pattern at 6.1 MHz.

Pattern  
Calculated  
Pattern  
Measured



Azimuth Angle Degrees.

Figure 7



# Log-periodic Monopole Antenna Azimuth Pattern at 7.1 MHz.

Pattern  
Calculated  
 Pattern  
Measured

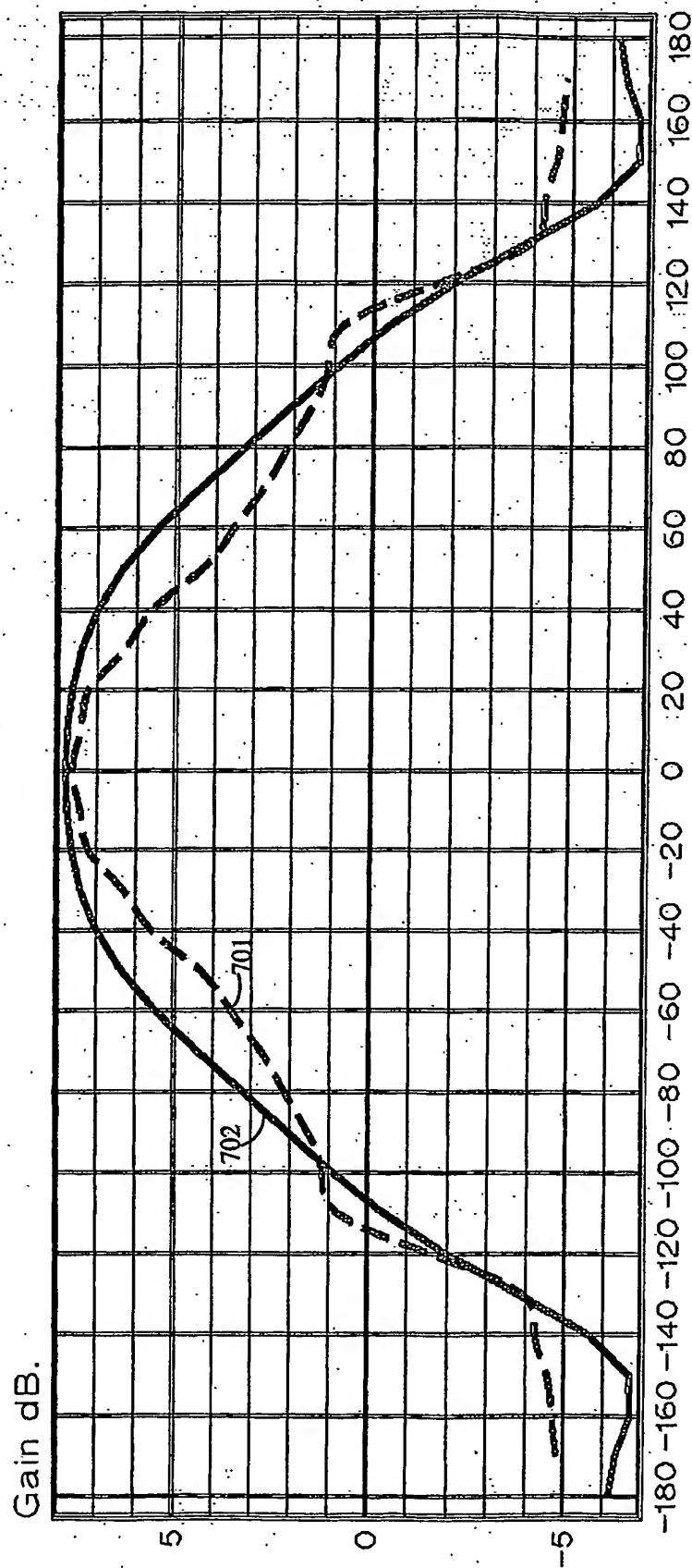


Figure 8

# Log-periodic Monopole Antenna. Azimuth Pattern at 8.1 MHz.

Pattern  
Calculated

Pattern  
Measured

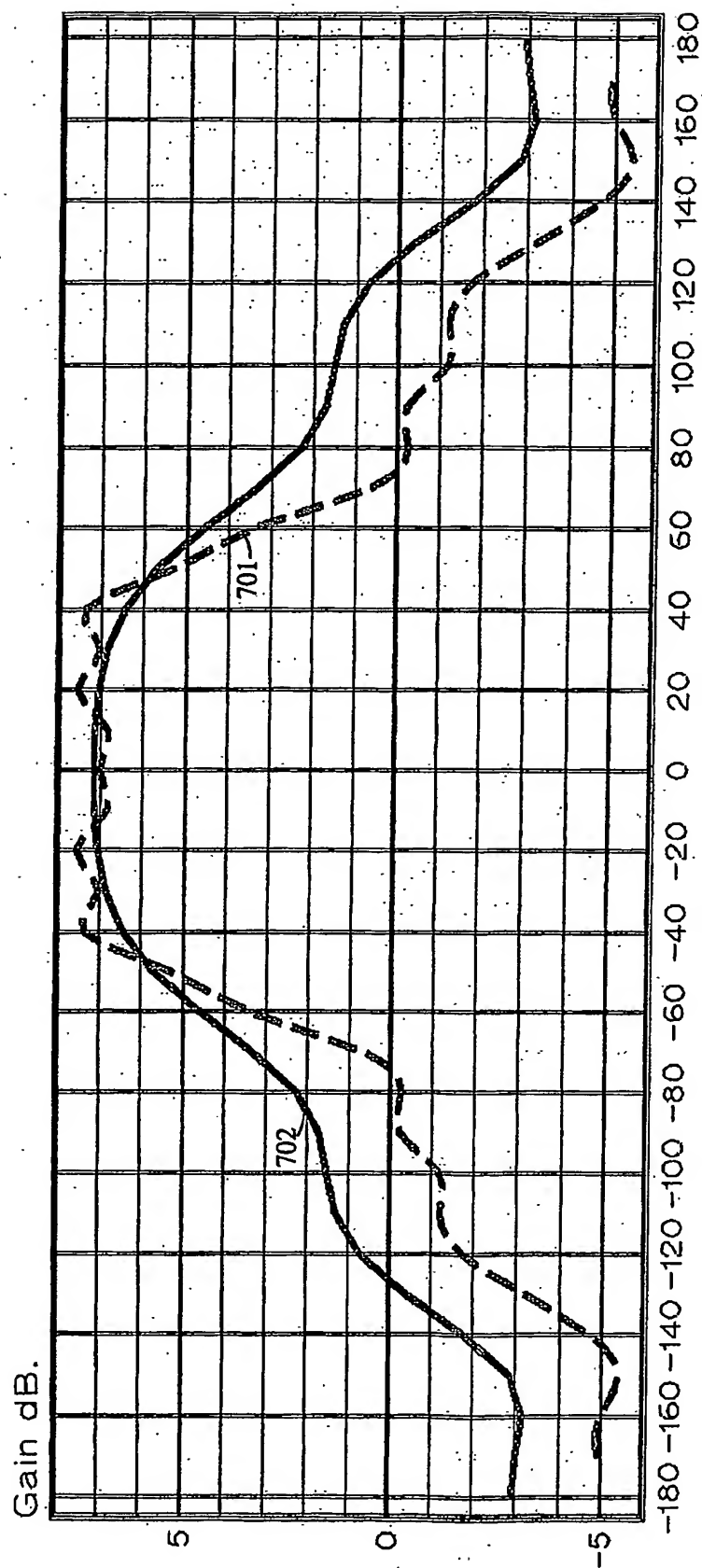


Figure 9

# Log-periodic Monopole Antenna Azimuth Pattern at 9.1 MHz.

Pattern  
Calculated

Pattern  
Measured

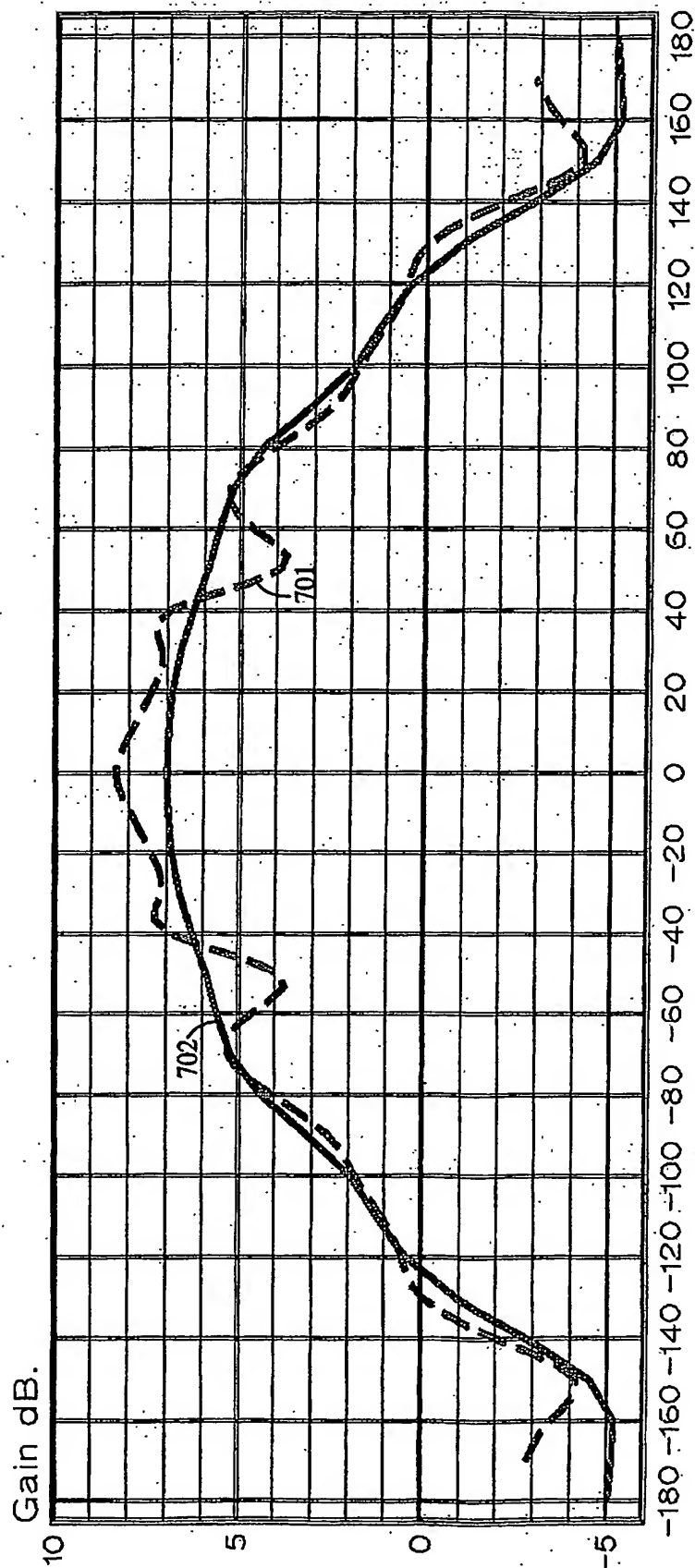


Figure 10

# Log-periodic Monopole Antenna Azimuth Pattern at 10.1 MHz.

Pattern  
Calculated  
 Pattern  
Measured

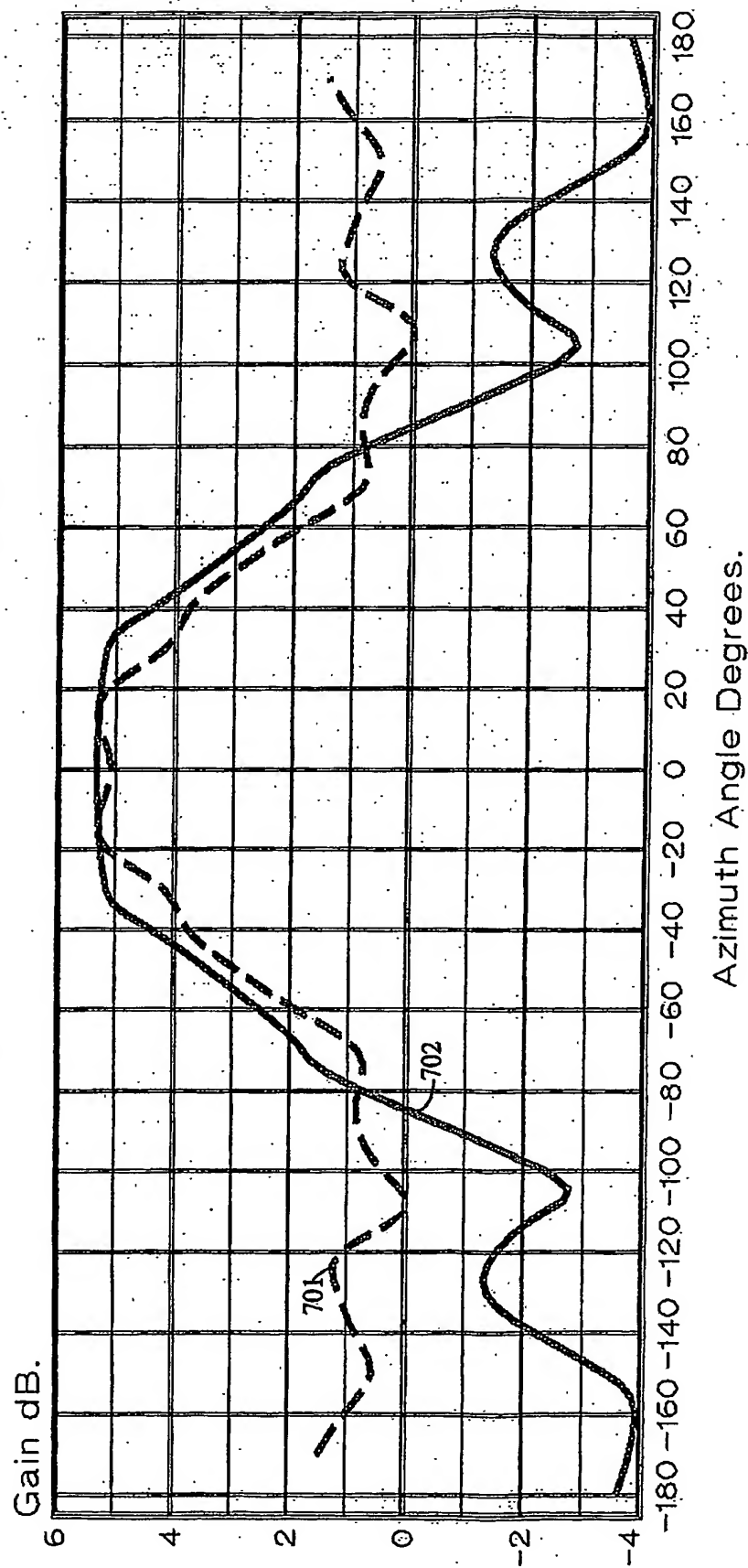


Figure 11

**This Page is Inserted by IFW Indexing and Scanning  
Operations and is not part of the Official Record**

**BEST AVAILABLE IMAGES**

- Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

☒ **BLACK BORDERS**

☐ **IMAGE CUT OFF AT TOP, BOTTOM OR SIDES**

☒ **FADED TEXT OR DRAWING**

☒ **BLURRED OR ILLEGIBLE TEXT OR DRAWING**

☐ **SKEWED/SLANTED IMAGES**

☐ **COLOR OR BLACK AND WHITE PHOTOGRAPHS**

☐ **GRAY SCALE DOCUMENTS**

☐ **LINES OR MARKS ON ORIGINAL DOCUMENT**

☐ **REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY**

☐ **OTHER:** \_\_\_\_\_

**IMAGES ARE BEST AVAILABLE COPY.**

**As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.**